

# Efekti primjene prirodnog gasa pri sagorijevanju čvrstih goriva u letu - *reburning* tehnologija

## Effects of Natural Gas Application in Combustion of Pulverized Solid Fuels - *Reburning* Technology

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**Rezime** - U sadašnjem vremenu je, istovremeno projicirano i za blisko buduće vremensko razdoblje, na globalnom nivou veoma izražena energetska tranzicija koja u osnovi podrazumijeva fazno i značajno smanjenje primjene fosilnih goriva, naročito uglja u energetici i industriji, sve do konačnog prestanka te primjene. Na tom putu energetske tranzicije, sve značajniju ulogu generalno dobijaju obnovljivi izvori energije te alternativna goriva, pri čemu su, paralelno tome, i zahtjevi prema energetskim sistemima u pogledu povećanja energetske efikasnosti i okolinske prihvatljivosti neizostavni kriteriji. S tim u vezi se naročit napor usmjerava na proširenje portfolija primarnih goriva u postojećim velikim energetskim sistemima kakve su npr. termoelektrane na uglj. Stoga se danas u velikim kotlovima, s ciljem i smanjenja emisije  $\text{NO}_x$ , skoro pa neizostavno primjenjuje stepenovani privod vazduha za sagorijevanje kao primarna mjera u ložištu (*air staging*). Uz prethodnu mjeru, veoma brojni su primjeri i stepenovanog privoda osnovnog goriva u zonu sagorijevanja (*fuel staging*), te ipak manji broj primjera primjene trećeg ili dodatnog goriva, kakva je npr. primjena biogasa ili prirodnog gasa pri sagorijevanju osnovnog čvrstog goriva u letu (*reburning technology*). U opštem slučaju, ovim mjerama istovremeno se povećava efikasnost konverzije primarne energije iz goriva i smanjuje emisija nepoželjnih komponenti u okolinu. Do koje mjere su izraženi prethodni efekti pri primjeni prirodnog gasa kod sagorijevanja bosanskohercegovačkog uglja i otpadne drvene biomase, pokaza-no je u ovom radu kroz rezultate obavljenih istraživanja: pri takvom sagorijevanju dolazi do dodatnog smanjenja emisije  $\text{NO}_x$  i to proporcionalno udjelu gasa - pri procesnoj temperaturi  $1350\text{ }^\circ\text{C}$  i pri 10% energetskog udjela gasa pri sagorijevanju sa ugljem, u odnosu na emisiju bez primjene dodatnog goriva, evidentirano je smanjenje emisije  $\text{NO}_x$  za više od  $250\text{ mg/m}_n^3$ .

**Ključne riječi** - uglj, drvena biomasa, prirodni gas, sagorijevanje, emisija  $\text{NO}_x$ .

**Abstract** - The energy transition basically implies a phased and significant reduction in the use of fossil fuels, until the final cessation of use in the near future. Renewable energy sources and alternative fuels are an increasingly important part of the energy transition. At the same time, it is necessary that energy systems increase energy efficiency and environmental

acceptability. In this regard, great efforts are being made to expand the portfolio of primary fuels in existing large energy systems, e.g. thermal power plants. Therefore, today in large boilers, in order to reduce  $\text{NO}_x$  emission, staged air supply for combustion is inevitably used as the primary measure in the furnace (*air staging*). In addition to the previous measure, there are many examples of staged fuel supply to the combustion zone (*fuel staging*), and still a small number of examples of the use of third or additional fuel, e.g. application of biogas or natural gas in combustion of pulverized solid fuels (*reburning technology*). General, these measures simultaneously increase the efficiency of primary energy conversion from fuel and reduce the emission of undesirable components into the environment. The results of this paper show the extent to which the effects of the use of natural gas in the co-firing of Bosnian coal and waste wood biomass are expressed. In this process there is an additional reduction of  $\text{NO}_x$  in proportion to the share of gas - at a process temperature of  $1350\text{ }^\circ\text{C}$  and at 10% of the energy content of gas in combustion with coal, compared to emissions without additional fuel, recorded reduction of  $\text{NO}_x$  emissions by more than  $250\text{ mg/m}_n^3$ .

**Index Terms** - Coal, Wood biomass, Natural gas, Combustion,  $\text{NO}_x$  emissions

### I INTRODUCTION

The introduction of renewable fuels into regular operation, with the aim of decarbonisation or reduction of  $\text{CO}_2$  emissions, such as waste wood biomass, is a complex and quite demanding process, not only due to the necessary technical interventions at an existing plant, but also unknowns to which such activities can result in the given concept of the furnace, i.e. the boiler. These unknowns are particularly pronounced in the combustion of mixtures of different fuels, including the behaviour of the mineral part of the fuel in this process, and the impact of this process on the environment, i.e. the emission of polluting components of flue gases. Some of these potential problems were detected in the re-search presented in [1]. Despite the previous, due to the necessity and importance of implementing the energy transition towards decarbonisation in the world, so far there are a large number of examples of energy plants adapted to the simultaneous use of different fuels (fossil,

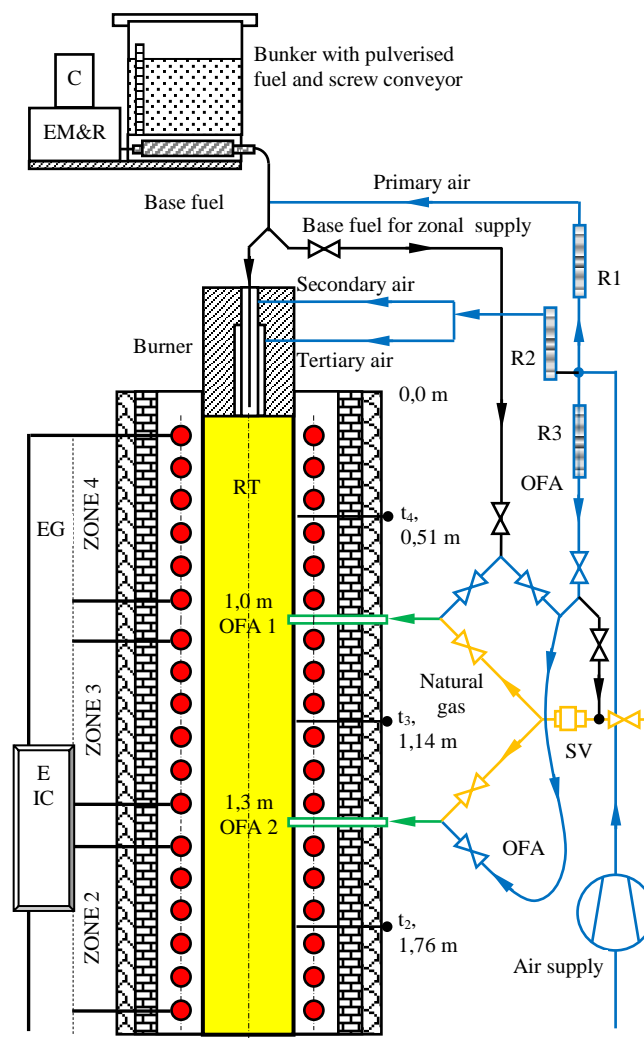
renewable and even alternative) in regular operation. Thus, for example, co-firing of coal and waste wood biomass or biomass residues from agricultural activity by the middle of the last decade put into regular operation in over 230 thermal power plants across the European Union (EU), [2]. On the other hand, a significant reduction in NO<sub>x</sub> emissions, compared to conventional combustion systems, can be achieved by using newer generation burners (vortex or flow Low NO<sub>x</sub> burners - LNB), graduated air combustion air supply (air staging, Over Fire Air - OFA), gradual introduction of basic fuel into the furnace (fuel staging), installation of double-row or multi-row burners observed by the height of the furnace and the use of additional fuels and their introduction into the furnace subsequently (eg. natural gas, biogas) - reburning technology. LNB burners work on the principle of zone or staged supply of combustion air observed at the level of a single burner - these burners result in a significant reduction in NO<sub>x</sub> emissions and as such are practically indispensable equipment in the design and construction of new energy boilers. Also, these burners are widely used for existing solid fuel boilers as a replacement for conventional flow-type burners, [3]. The scientific paper [4] presents the results and effects of staged air supply on NO<sub>x</sub> emissions - dried lignite was used as fuel. It has been shown that in this way there is a significant reduction in NO<sub>x</sub> emissions - the results relate to the study of the influence of excess air coefficient, combustion air distribution and the distance of the OFA portion of air into the reaction zone relative to the burner. Similar to the previous one, reference [5] states that, with Low-NO<sub>x</sub> burners, NO<sub>x</sub> emissions can be reduced by one-fifth, but that, due to the high combustion temperature, these emissions are still high (1036 mg/m<sup>3</sup> at 6% O<sub>2</sub> in dry flue gases), and for further reduction of NO<sub>x</sub> emissions, a zone or staged air supply - OFA is recommended. Also, the positive effect of staged air supply on NO<sub>x</sub> emission reduction is presented in references [6-7] where the results refer to coal combustion, as well as in references [8-12] for the case of co-firing coal and bio-mass. The paper [13] presents interesting results of research on coal combustion as a basic fuel with subsequent reburning of different types of waste wood biomass with an emphasis on the application of such a measure in the furnace to NO<sub>x</sub> emissions.

By subjecting coal blends, as well as mixtures of coal and waste woody biomass, to combustion at different temperatures with the application of staged combustion air supply as primary measure, and with the introduction of a portion of the OFA air at different distances from the primary burner and with the natural gas as third fuel, it is possible to determine the appropriate response of the combustion process through the measurement of process parameters and their analysis, i.e. it is possible to come to relevant conclusions about the impact of the location of the introduction of the OFA air and the application of natural gas to the process itself, and consequently the effect on the emission of flue gas components into the environment (CO<sub>2</sub>, CO, NO<sub>x</sub>, and SO<sub>2</sub>). Based on these conclusions it is possible to quantify and sublimate the characteristics of co-firing coal with woody biomass and natural gas, including the advantages of conversion of primary energy from fuels under conditions of solid fuel pulverized combustion technology with a staged combustion air supply, [2]. In this case, the total combustion air is divided into

four streams or portions: primary, secondary, tertiary and OFA - see the picture of the experimental plant given behind.

## II EXPERIMENTAL SET-UP

**Experimental line:** Automatic Controlled Tube Reactor experimental plant has been installed at Laboratory for Coal and Biomass Combustion (University of Sarajevo - Faculty of Mechanical Engineering, Department of Energy). This plant enables testing of combustion characteristics of different fuels under different ambient and technological conditions. Principal schema of the upper part of the plant with designated ancillary systems for classical and stepped fuel supply (basic and additional fuel) and zone or stepped supply of combustion air to the reaction pipe is given in Figure 1. - see also [2] and [14-16].



**Figure 1.** Principal scheme of the experimental plant: Upper part of the experimental plant with designated systems for classical and stepped fuel supply (basic and additional fuel) and zone or stepped combustion air supply to the reaction tube (RT) - *air staging, fuel staging, reburning technology*

Briefly, the plant is designed to operate in a wide temperature range (from ambient temperature to 1560 °C) and in conditions of different amount and distribution of basic fuel and air

combustion, including the possibility of testing *reburning* combustion technologies using additional fuel, such as natural gas. Basically, the research provides data related to combustion efficiency, deposition intensity and characteristics of deposits from the reaction zone as well as slag and ash at the reactor outlet, and emissions of flue gas components: O<sub>2</sub>, CO, CO<sub>2</sub>, NO, NO<sub>2</sub>, NO<sub>x</sub> i SO<sub>2</sub>, [2].

**Mixtures of solid fuels for research:** For the purpose of experimental research on the effects of natural gas on the combustion characteristics of pulverized solid fuels (coal mixtures or mixtures coal and waste woody biomass) in terms of emissions of flue gas components into the environment, especially nitrogen oxides (NO<sub>x</sub>=NO+NO<sub>2</sub>), the following matrix of basic test mixtures of solid fuels was formed, [2] - Table 1:

- The coal mixtures that has been fired in TPP Kakanj for the last few years - fuel label: U100. This coal blend was produced by mixing coals delivered to the coal depot of TPP Kakanj from several mines (Kakanj, Breza, Zenica, Gracanica, Livno, Nova Bila, Banovići, etc.) in approximately the same percentage as they are delivered from the mentioned mines. For laboratory testing purposes a sample of this coal mixture (coal powder) is excluded directly behind the mills during real operation of the Unit 5 in TPP Kakanj.
- Mixtures of previous test fuel U100 and waste wood biomass (sawdust) **B100** - fuel code: **U95B5**, mixture in which the mass fraction of coal U100 95% and biomass **B100** 5%. The sawdust is a mixture of beech and spruce formed during the primary processing of wood, in an approximate ratio of 1: 1 by weight. This test fuel (**U95B5**) was also excluded in the operation behind the mills of block 5 in TPP Kakanj.
- A mixture of brown coal from the mines Kakanj, Breza and Zenica in a mass ratio of 70:20:10, respectively - fuel designation: **K70B20Z10**. This coal mixture was formed after drying and grinding the components in a laboratory mill.

**Table 1.** Basic properties of test fuel, [15]

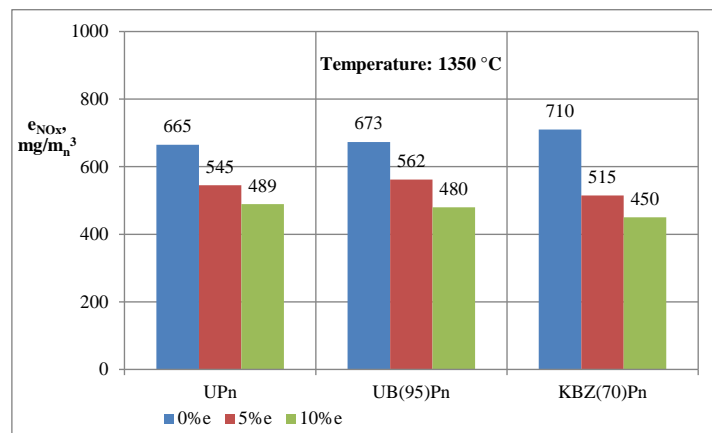
Fuel/Label	U100	U95B5	K70B20Z10
Moisture, %	13.90	19.06	10.71
Ash, %	37.88	34.33	40.84
Volatiles, %	28.97	29.32	27.71
C <sub>fix</sub> , %	19.25	17.28	20.73
Combustible, %	48.22	46.60	48.44
Carbon, %	36.62	32.12	34.48
Hydrogen, %	2.60	2.20	2.33
Sulfur, %	2.06	1.57	2.41
Nitrogen, %	0.72	0.81	0.75
Oxygen, %	10.22	9.91	8.48
HHV, kJ/kg	13351	12651	13898
LHV, kJ/kg	12496	11759	13171

**Basic settings of test regimes:** The previously mentioned test solid fuels (mixtures of coal and a mixture of coal and wood biomass) were subjected to a laboratory investigation of combustion under the conditions of staged supply of combustion air into the combustion chamber and with natural gas as additional fuel. Test

regimes are defined and performed in the range of process temperatures corresponding to the temperatures from the real boiler operation in TPP Kakanj - pulverized-fuel technology with slag tap furnace: 1350÷1450 °C. The set of research aimed to gain as much knowledge about the characteristics of co-firing coal and biomass in the conditions of *reburning* technology with natural gas with a particular emphasis on emissions of flue gas components, primarily NO<sub>x</sub>. Test regimes of co-firing with natural gas as an additional fuel, were performed with 5% and 10% energy content of gas. These test tests for natural gas combustion were assigned fuel designations: UPn, UB(95)Pn i KBZ70Pn, where "n" represents the energy share of natural gas in the total energy input into the furnace through fuel. In all test regimes, the total coefficient of excess air was λ=1.15 while the distribution of that total air was with the ratio λ<sub>1</sub>/λ=0.95/1.15 - a substoichiometric amount of air is supplied to the burner, λ<sub>1</sub>=0.95.

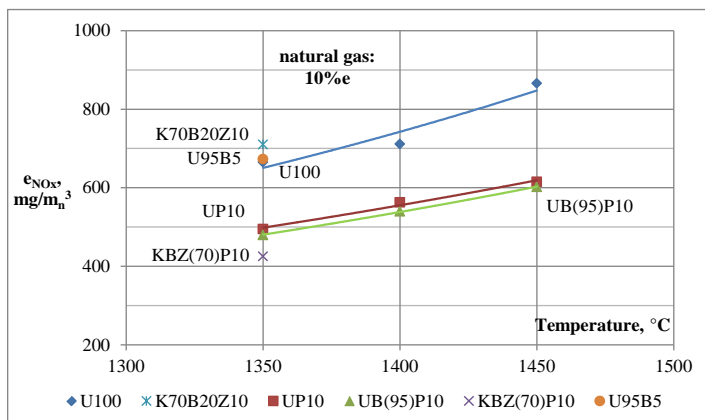
### III RESEARCH RESULTS WITH DISCUSSION

The effects of the use of natural gas as a fuel reburning on NO<sub>x</sub> emissions during the pulverized combustion of these test solid fuels and at a combustion process temperature of 1350 °C are shown in the following Figure 2. At the same time, for the given solid fuels, the NO<sub>x</sub> emission values for the case of 0%, 5% and 10% of the share of natural gas in combustion are also given - observed by the share in the total energy input into the furnace. In general, in relation to NO<sub>x</sub> emissions without the use of gas as an additional fuel (0%e), a decrease in that emission was recorded. For example, NO<sub>x</sub> emissions from the combustion of U100 fuel when reburning with 5%e gas are lower by 120 mg/m<sup>3</sup> or 18%, while the same emission at 10%e energy content of gas is lower by more than 170 mg/m<sup>3</sup> or by about 27%. The situation is similar with the co-firing of coal and biomass with natural gas – fuel UB(95)Pn: at 10%e gas content, NO<sub>x</sub> emissions are lower by approx. 29%. It is important to note that NO<sub>x</sub> emissions from co-firing coal and biomass are practically at the level of emissions from coal combustion - compare NO<sub>x</sub> emissions for fuels U100 and U95B5 in Figure 2 and then related emissions from firing of the same fuels but with natural gas (fuels marked UPn and UB (95) Pn).



**Figure 2.** NO<sub>x</sub> emissions at a combustion process temperature of 1350 °C for fuels of different composition and when using natural gas as an additional fuel - *reburning* technology

Similarly, the effects of natural gas on  $\text{NO}_x$  emissions in combustion of pulverized solid fuels but as a function of process temperature are presented in the following Figure 3, with all results referring to the case when the energy content of combustion gas is 10%. This diagram also shows the  $\text{NO}_x$  emission values when burning basic test fuels (without natural gas) at 1350 °C - compare the values with Figure 2, but also the emission values at 1400 °C and 1450 °C for U100 fuel. Thus, it can be seen in the diagram that the  $\text{NO}_x$  emission for reburning technology with natural gas in the entire considered temperature range is compared with the emission measured during the combustion of U100 coal mixture without the use of natural gas. For example, it is noticeable that the  $\text{NO}_x$  emission for U100 fuel with reburning technology with 10%e gas content (UP10) and at temperature of 1450 °C is 615  $\text{mg}/\text{m}_n^3$ , which is approximately 30% lower emission compared to the comparative emission without application natural gas. Also, the co-firing of coal and waste woody biomass in these conditions (UB(95)P) and at a temperature of 1450 °C measured emissions of 602  $\text{mg}/\text{m}_n^3$ , which is practically the same 30% less than the emissions from combustion only coal marked U100 (866  $\text{mg}/\text{m}_n^3$ ), [2].



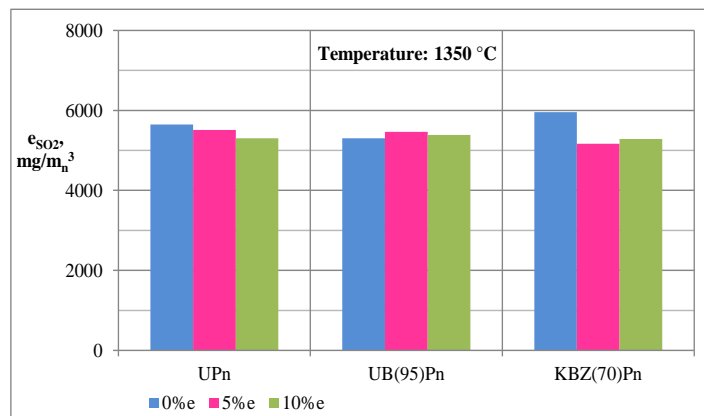
**Figure 3.** Effects of natural gas application on  $\text{NO}_x$  emissions at variable process temperature and co-firing of solid fuels of different composition - reburning technology

Other effects of natural gas application on the combustion characteristics of the subject fuels were investigated during these test regimes. For example, the impact of natural gas as a fuel reburning on  $\text{SO}_2$  emissions during the combustion of basic test solid fuels at a combustion process temperature of 1350 °C was qualitatively detected - see the results of the research in the following Figure 4.

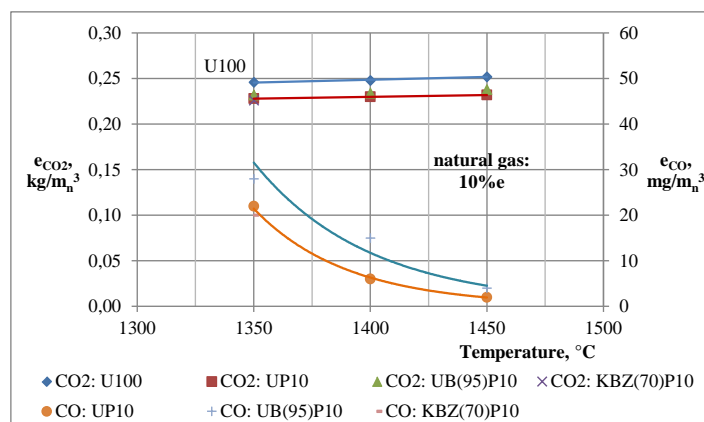
In general, combustion in such conditions and with regard to the level of that emission, there is a practically insignificant reduction in  $\text{SO}_2$  emissions. For example  $\text{SO}_2$  emissions from reburning with 10%e of natural gas are on average about 325  $\text{mg}/\text{m}_n^3$  lower than  $\text{SO}_2$  emissions from the combustion of U100 coal mixtures.

At the same time, in all these test regimes of co-firing with natural gas, a very low level of incomplete combustion was recorded, validated through CO emissions, especially in combustion of basic fuels of smaller granulation and combustion process temperature above 1400 °C - in these cases CO emissions

are practically negligible, below 5  $\text{mg}/\text{m}_n^3$  - see the results in Figure 5.



**Figure 4.**  $\text{SO}_2$  emissions at a combustion process temperature of 1350 °C for fuels of different composition and when using natural gas as an additional fuel - reburning technology



**Figure 5.** Effects of natural gas application on  $\text{CO}_2$  and CO emissions at variable process temperature and co-firing of solid fuels of different composition - reburning technology

The above phenomenon can be explained by a very violent reaction, i.e. the combustion of natural gas in the reaction zone of re-burning (reburning zone) in which the local temperature rises, which further burns  $C_{\text{fix}}$  in solid fuel particles and incomplete combustion products (such as CO and/or  $C_mH_n$ ) which occurred in the primary combustion zone in which there is a lack of combustion air (from the burner outlet to the place of introduction of OFA air portion is  $\lambda < 1$ , substoichiometric zone), [2]. It is also known that the combustion of natural gas, in relation to the combustion of liquid and especially solid fuels, is accompanied by the lowest  $\text{CO}_2$  emissions. This was reflected in previous results in the set of subject test regimes for combustion of selected solid fuels with reburning technology with natural gas - see Figure 5 and compare  $\text{CO}_2$  emission values during reburning with gas (e.g. fuel UP10, UB(95)P10) in relation to  $\text{CO}_2$  emissions generated during the co-firing of coal mixtures without the use of natural gas - fuel marked U100. During reburning,  $\text{CO}_2$  emissions average about 0.231  $\text{kg}/\text{m}_n^3$  and are



lower by almost  $0.020 \text{ kg/m}_n^3$  compared to emissions from the co-firing of U100 coal mixture without the use of natural gas.

In parallel with the previous determination of the values and emission levels of essential components in flue gases, during the test regimes the quantified behaviour of the mineral part from fuel (ash) in the given ambient and technical-technological settings of combustion of pulverized solid fuels (coal, woody biomass) and when using natural gas as an additional fuel for subsequent co-firing - *reburning* technology. In this regard, for the purpose of visual and appropriate chemical analysis, samples of ash deposits were collected from the reaction tube, which, during combustion, are collected on uncooled ceramic tablets and samples of slag and fly ash from the bottom of the reactor. In this regard, as an example, the following Figure 6 shows the exempted deposit from tablets and slag from the bottom of the furnace in the co-firing of coal and waste woody biomass U95B5 in terms of reburning technology with 5% natural gas and process temperature of  $1400 \text{ }^\circ\text{C}$  - the fuel designation for this test mode is UB(95)P5.



**Figure 6.** Basic test mode settings: UB(95)P5,  $1400 \text{ }^\circ\text{C}$ ,  $\lambda_1/\lambda=0.95/1.15$ ; ash deposit on ceramic tablet - left, slag from reactor bottom/furnace - right

Compared to other solid samples of coal combustion products and waste wood biomass, with a different share of biomass in the mixture and at the same process temperature, in which, as in this case, are also quite similar larger molten deposits, and it can be concluded that intensification of slagging at this combustion temperature should not be associated with the content of woody biomass in the mixture. In this case, too, the reburning technology has the same form and structure of deposits as in the test regimes without the use of natural gas. Namely, the initial formation of larger molten deposits at a combustion temperature of  $1400 \text{ }^\circ\text{C}$  can further escalate because new layers accumulate on these initial molten deposits and a stepped structure of hard molten deposits is formed. The tablet also contains a part of the deposit that is not fused - see previous Figure 6. Therefore, comparing the condition and structure of solid samples of combustion products for different fuels and for different temperature and technical-technological conditions of combustion, it can be concluded that natural gas does not worsen the state of the combustion process from the aspect of the behaviour of solid fuel ash in that process.

#### IV CONCLUSION

The purpose of this paper is to present the effects of simultaneous use of natural gas in the process of combustion of

pulverized solid fuels, and to present the results of research on applied reburning technology at the experimental plant. Based on the obtained and partially presented research results, the following concrete conclusions can be made regarding the effects of natural gas as an additional fuel on the emission of flue gas components during co-firing of various mixtures of coal and waste woody biomass:

- When reburning co-firing with natural gas as an additional fuel, the  $\text{NO}_x$  emission is reduced - this reduction is proportional to the share of natural gas that is subsequently introduced into the reaction zone. For example, at a process temperature of  $1350 \text{ }^\circ\text{C}$  and at 10% energy content of gas, in relation to emissions without additional fuel, a reduction in  $\text{NO}_x$  emissions by more than  $250 \text{ mg/m}_n^3$  was recorded -  $\text{NO}_x$  emissions for coal mixtures K70B20Z10 reduced from 710 to  $450 \text{ mg/m}_n^3$  or about 37%.
- When co-firing coal-biomass mixture with natural gas as additional fuel (UB(95)P10) at temperature of  $1450 \text{ }^\circ\text{C}$ , the measured  $\text{NO}_x$  emission is  $602 \text{ mg/m}_n^3$ , which is about 30% less than emission with coal U100 which is  $866 \text{ mg/m}_n^3$ . At a combustion temperature of  $1350 \text{ }^\circ\text{C}$ , a  $\text{NO}_x$  emission of  $425 \text{ mg/m}_n^3$  was measured for the K70B20Z10 coal mixture, which is about 40% less than the comparative emission.
- When using the natural gas in reburning test regimes there is a slight decrease of  $\text{SO}_2$  emission. Burning the coal U100 with 10%e of natural gas, the  $\text{SO}_2$  emission is on average about  $325 \text{ mg/m}_n^3$  is lower than the  $\text{SO}_2$  emission when co-firing mixture coal only.
- In combustion regimes with natural gas, CO emission is very low, especially when at temperatures above  $1400 \text{ }^\circ\text{C}$ , where CO emissions are practically negligible: below  $5 \text{ mg/m}_n^3$ . In doing so,  $\text{CO}_2$  emissions are lower by almost  $0.020 \text{ kg/m}_n^3$  compared to emissions when combusting U100 coal mixture without natural gas.
- Primary measures in the furnace, staged air supply and reburning technologies with natural gas, do not have a negative impact on the process of formation and structure of deposits in the boiler and therefore do not worsen the tendency of base fuel ash, coal or coal mixture with waste woody biomass boiler heating surfaces.

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